

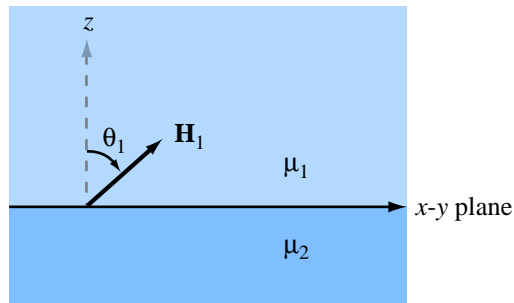
### Magnetic Boundary Conditions

**Problem/3** The  $x$ - $y$  plane separates two magnetic media with magnetic permeabilities  $\mu_1$  and  $\mu_2$ , as shown in Fig.3. If there is no surface current at the interface and the magnetic field in medium 1 is

$$\mathbf{H}_1 = \hat{x}H_{1x} + \hat{y}H_{1y} + \hat{z}H_{1z},$$

find:

- (a)  $\mathbf{H}_2$ ,
- (b)  $\theta_1$  and  $\theta_2$ , and
- (c) evaluate  $\mathbf{H}_2$ ,  $\theta_1$ , and  $\theta_2$  for  $H_{1x} = 2$  (A/m),  $H_{1y} = 0$ ,  $H_{1z} = 4$  (A/m),  $\mu_1 = \mu_0$ , and  $\mu_2 = 4\mu_0$ .



FigØ: Adjacent magnetic media.

**Solution:**

(a) From,

$$\mu_1 H_{1n} = \mu_2 H_{2n},$$

and in the absence of surface currents at the interface,

$$H_{1t} = H_{2t}.$$

In this case,  $H_{1z} = H_{1n}$ , and  $H_{1x}$  and  $H_{1y}$  are tangential fields. Hence,

$$\mu_1 H_{1z} = \mu_2 H_{2z},$$

$$H_{1x} = H_{2x},$$

$$H_{1y} = H_{2y},$$

and

$$\mathbf{H}_2 = \hat{\mathbf{x}}H_{1x} + \hat{\mathbf{y}}H_{1y} + \hat{\mathbf{z}}\frac{\mu_1}{\mu_2}H_{1z}.$$

(b)

$$H_{1t} = \sqrt{H_{1x}^2 + H_{1y}^2},$$

$$\tan \theta_1 = \frac{H_{1t}}{H_{1z}} = \frac{\sqrt{H_{1x}^2 + H_{1y}^2}}{H_{1z}},$$

$$\tan \theta_2 = \frac{H_{2t}}{H_{2z}} = \frac{\sqrt{H_{1x}^2 + H_{1y}^2}}{\frac{\mu_1}{\mu_2}H_{1z}} = \frac{\mu_2}{\mu_1} \tan \theta_1.$$

(c)

$$\mathbf{H}_2 = \hat{\mathbf{x}}2 + \hat{\mathbf{z}}\frac{1}{4} \cdot 4 = \hat{\mathbf{x}}2 + \hat{\mathbf{z}} \quad (\text{A/m}),$$

$$\theta_1 = \tan^{-1}\left(\frac{2}{4}\right) = 26.56^\circ,$$

$$\theta_2 = \tan^{-1}\left(\frac{2}{1}\right) = 63.44^\circ.$$

**Problem/4** Given that a current sheet with surface current density  $\mathbf{J}_s = \hat{\mathbf{x}}8$  (A/m) exists at  $y = 0$ , the interface between two magnetic media, and  $\mathbf{H}_1 = \hat{\mathbf{z}}11$  (A/m) in medium 1 ( $y > 0$ ), determine  $\mathbf{H}_2$  in medium 2 ( $y < 0$ ).

**Solution:**

$$\mathbf{J}_s = \hat{\mathbf{x}}8 \text{ A/m},$$

$$\mathbf{H}_1 = \hat{\mathbf{z}}11 \text{ A/m}.$$

$\mathbf{H}_1$  is tangential to the boundary, and therefore  $\mathbf{H}_2$  is also. With  $\hat{\mathbf{n}}_2 = \hat{\mathbf{y}}$ , we have

$$\hat{\mathbf{n}}_2 \times (\mathbf{H}_1 - \mathbf{H}_2) = \mathbf{J}_s,$$

$$\hat{\mathbf{y}} \times (\hat{\mathbf{z}}11 - \mathbf{H}_2) = \hat{\mathbf{x}}8,$$

$$\hat{\mathbf{x}}11 - \hat{\mathbf{y}} \times \mathbf{H}_2 = \hat{\mathbf{x}}8,$$

or

$$\hat{\mathbf{y}} \times \mathbf{H}_2 = \hat{\mathbf{x}}3,$$

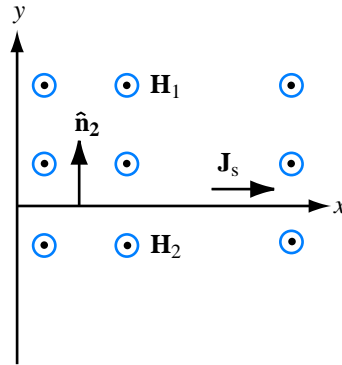


Fig04: Adjacent magnetic media with  $\mathbf{J}_s$  on boundary.

which implies that  $\mathbf{H}_2$  does not have an  $x$ -component. Also, since  $\mu_1 H_{1y} = \mu_2 H_{2y}$  and  $\mathbf{H}_1$  does not have a  $y$ -component, it follows that  $\mathbf{H}_2$  does not have a  $y$ -component either. Consequently, we conclude that

$$\mathbf{H}_2 = \hat{z}3.$$

**Problem/3** In Fig."5," the plane defined by  $x - y = 1$  separates medium 1 of permeability  $\mu_1$  from medium 2 of permeability  $\mu_2$ . If no surface current exists on the boundary and

$$\mathbf{B}_1 = \hat{x}2 + \hat{y}3 \quad (\text{T}),$$

find  $\mathbf{B}_2$  and then evaluate your result for  $\mu_1 = 5\mu_2$ . Hint: Start out by deriving the equation for the unit vector normal to the given plane.

**Solution:** We need to find  $\hat{n}_2$ . To do so, we start by finding any two vectors in the plane  $x - y = 1$ , and to do that, we need three non-collinear points in that plane. We choose  $(0, -1, 0)$ ,  $(1, 0, 0)$ , and  $(1, 0, 1)$ .

Vector  $\mathbf{A}_1$  is from  $(0, -1, 0)$  to  $(1, 0, 0)$ :

$$\mathbf{A}_1 = \hat{x}1 + \hat{y}1.$$

Vector  $\mathbf{A}_2$  is from  $(1, 0, 0)$  to  $(1, 0, 1)$ :

$$\mathbf{A}_2 = \hat{z}1.$$

Hence, if we take the cross product  $\mathbf{A}_2 \times \mathbf{A}_1$ , we end up in a direction normal to the given plane, from medium 2 to medium 1,

$$\hat{n}_2 = \frac{\mathbf{A}_2 \times \mathbf{A}_1}{|\mathbf{A}_2 \times \mathbf{A}_1|} = \frac{\hat{z}1 \times (\hat{x}1 + \hat{y}1)}{|\mathbf{A}_2 \times \mathbf{A}_1|} = \frac{\hat{y}1 - \hat{x}1}{\sqrt{1+1}} = \frac{\hat{y}}{\sqrt{2}} - \frac{\hat{x}}{\sqrt{2}}.$$

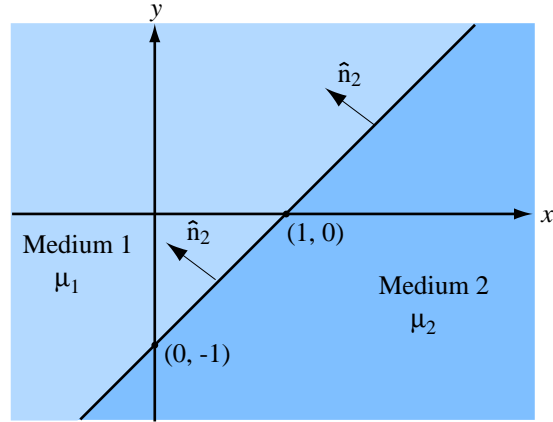


Fig.3: Magnetic media separated by the plane  $x - y = 1$

In medium 1, normal component is

$$B_{1n} = \hat{n}_2 \cdot \mathbf{B}_1 = \left( \frac{\hat{y}}{\sqrt{2}} - \frac{\hat{x}}{\sqrt{2}} \right) \cdot (\hat{x}2 + \hat{y}3) = \frac{3}{\sqrt{2}} - \frac{2}{\sqrt{2}} = \frac{1}{\sqrt{2}},$$

$$\mathbf{B}_{1n} = \hat{n}_2 B_{1n} = \left( \frac{\hat{y}}{\sqrt{2}} - \frac{\hat{x}}{\sqrt{2}} \right) \cdot \frac{1}{\sqrt{2}} = \frac{\hat{y}}{2} - \frac{\hat{x}}{2}.$$

Tangential component is

$$\mathbf{B}_{1t} = \mathbf{B}_1 - \mathbf{B}_{1n} = (\hat{x}2 + \hat{y}3) - \left( \frac{\hat{y}}{2} - \frac{\hat{x}}{2} \right) = \hat{x}2.5 + \hat{y}2.5.$$

Boundary conditions:

$$B_{1n} = B_{2n}, \quad \text{or} \quad \mathbf{B}_{2n} = \frac{\hat{y}}{2} - \frac{\hat{x}}{2},$$

$$H_{1t} = H_{2t}, \quad \text{or} \quad \frac{B_{2t}}{\mu_2} = \frac{B_{1t}}{\mu_1}.$$

Hence,

$$\mathbf{B}_{2t} = \frac{\mu_2}{\mu_1} \mathbf{B}_{1t} = \frac{\mu_2}{\mu_1} (\hat{x}2.5 + \hat{y}2.5).$$

Finally,

$$\mathbf{B}_2 = \mathbf{B}_{2n} + \mathbf{B}_{2t} = \left( \frac{\hat{y}}{2} - \frac{\hat{x}}{2} \right) + \frac{\mu_2}{\mu_1} (\hat{x}2.5 + \hat{y}2.5).$$

For  $\mu_1 = 5\mu_2$ ,

$$\mathbf{B}_2 = \hat{y} \quad (\text{T}).$$

## Inductance and Magnetic Energy

**Problem/3<** Obtain an expression for the self-inductance per unit length for the parallel wire transmission line of Fig."3(a) in terms of  $a$ ,  $d$ , and  $\mu$ , where  $a$  is the radius of the wires,  $d$  is the axis-to-axis distance between the wires, and  $\mu$  is the permeability of the medium in which they reside.

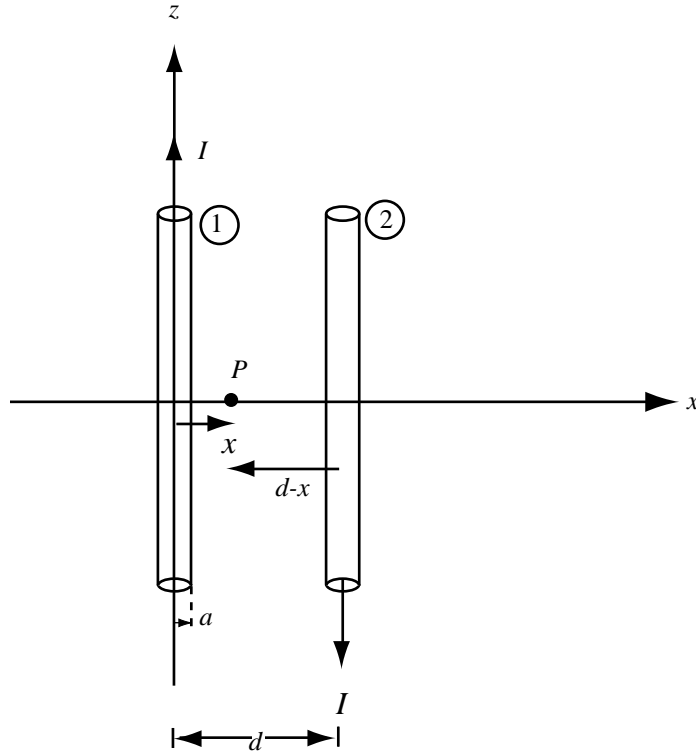
**Solution:** Let us place the two wires in the  $x$ - $z$  plane and orient the current in one of them to be along the  $+z$ -direction and the current in the other one to be along the  $-z$ -direction, the magnetic field at point  $P(x, 0, z)$  due to wire 1 is

$$\mathbf{B}_1 = \hat{\phi} \frac{\mu I}{2\pi r} = \hat{y} \frac{\mu I}{2\pi x},$$

where the permeability has been generalized from free space to any substance with permeability  $\mu$ , and it has been recognized that in the  $x$ - $z$  plane,  $\hat{\phi} = \hat{y}$  and  $r = x$  as long as  $x > 0$ .

Given that the current in wire 2 is opposite that in wire 1, the magnetic field created by wire 2 at point  $P(x, 0, z)$  is in the same direction as that created by wire 1, and it is given by

$$\mathbf{B}_2 = \hat{y} \frac{\mu I}{2\pi(d-x)}.$$



FigØ: Parallel wire transmission line.

Therefore, the total magnetic field in the region between the wires is

$$\mathbf{B} = \mathbf{B}_1 + \mathbf{B}_2 = \hat{\mathbf{y}} \frac{\mu I}{2\pi} \left( \frac{1}{x} + \frac{1}{d-x} \right) = \hat{\mathbf{y}} \frac{\mu I d}{2\pi x(d-x)}.$$

the flux crossing the surface area between the wires over a length  $l$  of the wire structure is

$$\begin{aligned} \Phi &= \iint_S \mathbf{B} \cdot d\mathbf{s} = \int_{z=z_0}^{z_0+l} \int_{x=a}^{d-a} \left( \hat{\mathbf{y}} \frac{\mu I d}{2\pi x(d-x)} \right) \cdot (\hat{\mathbf{y}} dx dz) \\ &= \frac{\mu I d}{2\pi} \left( \frac{1}{d} \ln \left( \frac{x}{d-x} \right) \right) \Big|_{x=a}^{d-a} \\ &= \frac{\mu I l}{2\pi} \left( \ln \left( \frac{d-a}{a} \right) - \ln \left( \frac{a}{d-a} \right) \right) \\ &= \frac{\mu I l}{2\pi} \times 2 \ln \left( \frac{d-a}{a} \right) = \frac{\mu I l}{\pi} \ln \left( \frac{d-a}{a} \right). \end{aligned}$$

Since the number of 'turns' in this structure is 1, the flux linkage is the same as magnetic flux:  $\Lambda = \Phi$ . The total inductance over the length  $l$  is

$$L = \frac{\Lambda}{I} = \frac{\Phi}{I} = \frac{\mu l}{\pi} \ln\left(\frac{d-a}{a}\right) \quad (\text{H}).$$

Therefore, the inductance per unit length is

$$L' = \frac{L}{l} = \frac{\mu}{\pi} \ln\left(\frac{d-a}{a}\right) \approx \frac{\mu}{\pi} \ln\left(\frac{d}{a}\right) \quad (\text{H/m}),$$

where the last approximation recognizes that the wires are thin compared to the separation distance (i.e., that  $d \gg a$ ). This has been an implied condition from the beginning of this analysis, where the flux passing through the wires themselves have been ignored.

**Problem/4** In terms of the d-c current  $I$ , how much magnetic energy is stored in the insulating medium of a 3-m-long, air-filled section of a coaxial transmission line, given that the radius of the inner conductor is 5 cm and the inner radius of the outer conductor is 10 cm?

**Solution:** the inductance per unit length of an air-filled coaxial cable is given by

$$L' = \frac{\mu_0}{2\pi} \ln\left(\frac{b}{a}\right) \quad (\text{H/m}).$$

Over a length of 2 m, the inductance is

$$L = 2L' = \frac{3 \times 4\pi \times 10^{-7}}{2\pi} \ln\left(\frac{10}{5}\right) = 416 \times 10^{-9} \quad (\text{H}).$$

From Eq. (5.106),  $W_m = LI^2/2 = 208I^2$  (nJ), where  $W_m$  is in nanojoules when  $I$  is in amperes. Alternatively, we can use Eq. (5.106) to compute  $W_m$ :

$$W_m = \frac{1}{2} \int_V \mu_0 H^2 dV.$$

From Eq. (5.106),  $H = B/\mu_0 = I/2\pi r$ , and

$$W_m = \frac{1}{2} \int_{z=0}^{3\text{m}} \int_{\phi=0}^{2\pi} \int_{r=a}^b \mu_0 \left(\frac{I}{2\pi r}\right)^2 r dr d\phi dz = 208I^2 \quad (\text{nJ}).$$